High-pressure structural and elastic properties of Ti2O3

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High-pressure structural and elastic properties of Tl$_2$O$_3$


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The structural properties of Thallium (III) oxide (Tl$_2$O$_3$) have been studied both experimentally and theoretically under compression at room temperature. X-ray powder diffraction measurements up to 37.7 GPa have been complemented with ab initio total-energy calculations. The equation of state of Tl$_2$O$_3$ has been determined and compared to related compounds. It has been found experimentally that Tl$_2$O$_3$ remains in its initial cubic bixbyite-type structure up to 22.0 GPa. At this pressure, the onset of amorphization is observed, being the sample fully amorphous at 25.2 GPa. The sample retains the amorphous state after pressure release. To understand the pressure-induced amorphization process, we have studied theoretically the possible high-pressure phases of Tl$_2$O$_3$. Although a phase transition is theoretically predicted at 5.8 GPa to the orthorhombic Rh$_2$O$_3$-II-type structure and at 24.2 GPa to the orthorhombic $\alpha$-Gd$_2$S$_3$-type structure, neither of these phases were observed experimentally, probably due to the hindrance of the pressure-driven phase transitions at room temperature. The theoretical study of the elastic behavior of the cubic bixbyite-type structure at high-pressure shows that amorphization above 22 GPa at room temperature might be caused by the mechanical instability of the cubic bixbyite-type structure which is theoretically predicted above 23.5 GPa. © 2014 AIP Publishing LLC. [http://dx.doi.org/10.1063/1.4897241]

I. INTRODUCTION

Thallium (III) oxide (Tl$_2$O$_3$) is a sesquioxide which occurs naturally as a rare mineral named avicennite. Tl$_2$O$_3$ crystallizes at ambient conditions in the body-centered cubic bixbyite-type structure with space group (S.G.) Ia-3, No. 206, $Z = 16$. Bixbyite-type Tl$_2$O$_3$ is isomorphic to the cubic structure of In$_2$O$_3$ and several rare-earth sesquioxides. Apart from the bixbyite-type structure, the corundum-type structure has been reported to be synthesized at high pressures above 23.5 GPa. © 2014 AIP Publishing LLC. [http://dx.doi.org/10.1063/1.4897241]

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The poisonous nature of thallium. In particular, contact with moisture and acids may form poisonous soluble thallium compounds, like thallium acetate, whose contact with skin should be avoided. Consequently, many properties of Tl$_2$O$_3$ are unknown. In particular, it was long thought that this compound behaves as a metallic conductor; however, it has been recently shown that it is a degenerate n-type semiconductor. This result is in good agreement with transport measurements which suggest that n-type conductivity comes from oxygen deficiency in the crystalline lattice. It is also in good agreement with optical measurements providing a band gap between 1.40 and 2.75 eV. Very little is known about the structural and mechanical properties of Tl$_2$O$_3$. The bulk moduli of both bixbyite-type and corundum-type structures are unknown. In this context, studies of Tl$_2$O$_3$ under compression could help in understanding its physical properties. In this work, we report an experimental and theoretical study of bixbyite-type Tl$_2$O$_3$ at room temperature and high-pressure (HP) by means of angle dispersive X-ray diffraction (AXD) and ab initio calculations. Technical aspects of the experiments and calculations are described in Secs. II and III, respectively. Results are presented and discussed in Sec. IV and conclusions summarized in Sec. V.
II. EXPERIMENTAL DETAILS

Commercial Tl₂O₃ powder with 99.99% purity (Sigma-Aldrich) was crushed in a mortar with a pestle to obtain a micron-sized powder. XRD measurements performed at 1 atm and room temperature with a Rigaku Ultima IV diffractometer (Cu Kα radiation) confirmed the bixbyite-type structure of Tl₂O₃.

HP-ADXRD experiments at room temperature up to 37.7 GPa were carried out at beamline I15 of the Diamond Light Source using a monochromatic X-ray beam (λ = 0.4246 Å) and a membrane-type diamond-anvil cell (DAC). Tl₂O₃ powder was loaded in a 150-μm diameter hole of an inconel gasket in a DAC with diamond-culet sizes of 350 μm. A 16:3:1 methanol-ethanol-water mixture was used as pressure-transmitting medium. A strip of gold was placed inside the gasket and used as the pressure sensor. Pressure was determined using the gold equation of state (EOS): B₀ = 167.5 GPa, and Bₙ = 5.79, whose parameters are obtained with a third-order Birch-Murnaghan equation. The X-ray beam was focused down to 30 × 30 μm² using Kickpatrick-Baez mirrors. A pinhole placed before the sample position was used as a clean-up aperture for filtering out the tail of the X-ray beam. The images were collected using a MAR345 image plate located at 350 mm from the sample. The diffraction patterns were integrated as a function of 2θ using FIT2D in order to give conventional, one-dimensional diffraction profiles. The indexing and refinement of the powder diffraction patterns were performed using the Unitcell, POWDERCELL, and GSAS program packages.

III. THEORETICAL CALCULATIONS

We have performed ab initio total-energy calculations within the density functional theory (DFT) using the plane-wave method and the pseudopotential theory with the Vienna ab initio simulation package (VASP). We have used the projector-augmented wave scheme (PAW) implemented in this package to take into account the full nodal character of the all-electron charge density in the core region. Basis set, including plane waves up to an energy cutoff of 520 eV were used in order to achieve highly converged results and accurate description of the electronic properties. The exchange-correlation energy was described with the generalized gradient approximation (GGA) with the PBEsol prescription. A dense special k-points sampling for the Brillouin zone (BZ) integration was performed in order to obtain very well-converged energies and forces. At each selected volume, the structures were fully relaxed to their equilibrium configuration through the calculation of the forces on atoms and the stress tensor. This allows obtaining the relaxed structures at the theoretical pressures defined by the calculated stress. In the relaxed equilibrium configurations, the forces on the atoms are less than 0.006 eV Å⁻¹, and deviations of the stress tensor from a diagonal hydrostatic form are less than 1 kbar (0.1 GPa). The application of DFT-based total-energy calculations to the study of semiconductor properties under HP has been reviewed in Ref. 29, showing that the phase stability, electronic, and dynamical properties of compounds under pressure are well described by DFT.

Ab initio calculations allow the study of the mechanical properties of materials. The elastic constants describe the mechanical properties of a material in the region of small deformations, where the stress-strain relations are still linear. The elastic constants can be obtained by computing the macroscopic stress for a small strain with the use of the stress theorem. Alternatively, the macroscopic stress can be also calculated using density functional perturbation theory (DFPT). In the present work, we perform the evaluation of the elastic constants of Tl₂O₃ with the use of the DFT as implemented in the VASP package. The ground state and fully relaxed structures were strained in different directions according to their symmetry. The total-energy variations were evaluated according to a Taylor expansion for the total energy with respect to the applied strain. Due to this fact, it is important to check that the strain used in the calculations guarantees the harmonic behavior. This procedure allows us to obtain the C₁₁ elastic constants in the Voigt notation. The number of independent elastic constants is reduced by crystalline symmetry.

IV. RESULTS AND DISCUSSION

A. X-ray diffraction and structural properties

The crystalline structure of cubic bixbyite-type Tl₂O₃ (see Fig. 1) has two different types of six-fold-coordinated thallium atoms. Thallium located at the 8b Wyckoff site has slightly distorted octahedral coordination while thallium located at 24d Wyckoff site has distorted trigonal prismatic coordination. Finally, oxygen atoms occupy 48e Wyckoff sites. From XRD measurements carried out at 1 atm and room temperature outside the DAC, we have made a Rietveld refinement of the lattice parameter and relative

![FIG. 1. Schematic representation of the crystalline structure of cubic bixbyite-type Tl₂O₃. The unit-cell and atomic bonds are shown. Oxygen corresponds to small (red) atoms while Tl(1) located at 8b and Tl(2) located at 24d correspond to light blue and dark blue atoms, respectively.](image-url)
atomic positions of the bixbyite-type structure. The refinement R-values are $R_p = 7.7\%$ and $R_{wp} = 10.2\%$. These results (summarized in Table I) are in quite a good agreement with those of Refs. 2–4, and with our calculations, all of them included in Table I for comparison.

Figure 2 shows ADXRD patterns of Tl$_2$O$_3$ up to 37.7 GPa. Diffractograms up to 22 GPa can be indexed with the cubic bixbyite-type Tl$_2$O$_3$ structure. The main difference between diffraction patterns up to 22 GPa is the shift of Bragg peaks to higher angles with pressure as the result of a unit-cell volume decrease. A typical peak broadening of Bragg peaks to higher angles with pressure as the result of a distortions caused by the appearance of defects which could be precursors of the pressure-induced amorphization (PIA) that will be commented later on.

From the refinement of the diffraction patterns up to 22 GPa, we obtained the pressure dependence of the Tl$_2$O$_3$ lattice parameter. In the Rietveld refinement, the oxygen atomic coordinates were supposed not to vary with pressure due to its small X-ray scattering cross section in comparison to that of thallium atom. Rietveld refinements carried out on HP-ADXRD data for Tl$_2$O$_3$ show that the $x$ fractional atomic coordinate of the Tl(2) atom up to 22 GPa was similar to that at 1 atm within experimental uncertainty. This result agrees with the weak pressure dependence of this atomic parameter obtained from our theoretical calculations (according to simulations, the $x$ fractional atomic coordinate of Tl(2) in Tl$_2$O$_3$

![FIG. 2. Room temperature XRD patterns of Tl$_2$O$_3$ at selected pressures. The background has not been subtracted. The diffractogram measured at 18.2 GPa is shown as empty circles. The calculated and difference XRD patterns at 18.2 GPa obtained from a Rietveld refinement are plotted with solid lines. The residuals at 18.2 GPa are $R_p = 7.7\%$ and $R_{wp} = 10.2\%$. Bragg reflections from Tl$_2$O$_3$ and gold are indicated with vertical ticks at 2.1 and 18.2 GPa. Gold reflections are marked with plus (+) symbols. The XRD pattern at 1 atm after releasing pressure is shown at the top.](image)

Table I. Structural parameters of bixbyite-type Tl$_2$O$_3$ at 1 atm.

<table>
<thead>
<tr>
<th>Parameter</th>
<th>X-ray diffraction$^a$</th>
<th>Ab initio PBEsol$^b$</th>
<th>Neutron diffraction$^c$</th>
<th>X-ray diffraction$^d$</th>
<th>Neutron diffraction$^e$</th>
</tr>
</thead>
<tbody>
<tr>
<td>$a$ (Å)</td>
<td>10.539(4)</td>
<td>10.6074</td>
<td>10.543</td>
<td>10.5344(3)</td>
<td>10.5363</td>
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<tr>
<td>Tl(1) site: 8b</td>
<td>$x = 0.25$</td>
<td>$x = 0.25$</td>
<td>$x = 0.25$</td>
<td>$x = 0.25$</td>
<td>$x = 0.25$</td>
</tr>
<tr>
<td></td>
<td>$y = 0.25$</td>
<td>$y = 0.25$</td>
<td>$y = 0.25$</td>
<td>$y = 0.25$</td>
<td>$y = 0.25$</td>
</tr>
<tr>
<td></td>
<td>$z = 0.25$</td>
<td>$z = 0.25$</td>
<td>$z = 0.25$</td>
<td>$z = 0.25$</td>
<td>$z = 0.25$</td>
</tr>
<tr>
<td>Tl(2) site: 24d</td>
<td>$x = 0.969(1)$</td>
<td>$x = 0.9667$</td>
<td>$x = 0.971(4)$</td>
<td>$x = 0.9681(22)$</td>
<td>$x = 0.9657(8)$</td>
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<tr>
<td></td>
<td>$y = 0$</td>
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<td>$y = 0$</td>
<td>$y = 0$</td>
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<tr>
<td></td>
<td>$z = 0.25$</td>
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<td>$z = 0.25$</td>
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<td>$z = 0.25$</td>
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<tr>
<td>O site: 48e</td>
<td>$x = 0.388(5)$</td>
<td>$x = 0.3829$</td>
<td>$x = 0.397(5)$</td>
<td>$x = 0.3824(17)$</td>
<td>$x = 0.3897(10)$</td>
</tr>
<tr>
<td></td>
<td>$y = 0.394(3)$</td>
<td>$y = 0.3885$</td>
<td>$y = 0.3776$</td>
<td>$y = 0.3905(15)$</td>
<td>$y = 0.3982(11)$</td>
</tr>
<tr>
<td></td>
<td>$z = 0.148(3)$</td>
<td>$z = 0.1540$</td>
<td>$z = 0.157(5)$</td>
<td>$z = 0.1542(18)$</td>
<td>$z = 0.1431(12)$</td>
</tr>
</tbody>
</table>

$^a$Our XRD measurements.
$^b$Our calculations.
$^c$Reference 2.
$^d$Reference 3.
$^e$Reference 4.
that the experimental value for $B_0$ in Tl$_2$O$_3$ ($B_0 = 156(3)$ GPa) is approximately 15\% smaller than that obtained for In$_2$O$_3$ ($B_0 = 184(10)$ GPa). In this comparison, we considered the EOS parameters obtained with a BM2 EOS with $B_0'$ fixed to 4 because the $B_0$ and $B_0'$ parameters are strongly correlated. The lower value of $B_0$ for cubic Tl$_2$O$_3$ when compared to that of In$_2$O$_3$ is consistent with the decrease of the bulk modulus of bixbyite-type sesquioxides when the ionic radius of the A cation increases in the series $A =$ In, Tl.

We note that bixbyite-type sesquioxides like In$_2$O$_3$ and Tl$_2$O$_3$ are much less compressible than sesquioxides of late group-15 elements in the Periodic Table like cubic $z$-Sb$_2$O$_3$ (S.G.: $Fd–3m$, No. 227, $Z = 16$) and monoclinic $z$-Bi$_2$O$_3$ (S.G.: $P2_1/c$, No. 14, $Z = 4$).

Figure 2 shows a drastic decrease of the intensity of the Bragg reflections of cubic Tl$_2$O$_3$ between 18.2 and 22 GPa. In addition, at 25.2 GPa, all the sharp crystalline peaks of cubic Tl$_2$O$_3$ disappear and two broad peaks appear at 8.75° and 11.53° (noted with asterisk marks). These two peaks remain up to 37.7 GPa, the maximum pressure achieved in our experiment and exhibit a small shift to higher angles between 25.2 and 37.7 GPa. These results can be interpreted as an amorphization of Tl$_2$O$_3$ above 22.0 GPa which is already completed at 25.2 GPa and will be discussed in Sec. IV B.

### B. Amorphization

It is commonly accepted that PLA in crystalline solids may occur if the crystalline structure becomes mechanical or dynamically unstable at a certain pressure; i.e., if mechanical stability criteria are violated or if the phonon dispersion curves contain imaginary frequencies for phonon modes at a given pressure. PLA due to these instabilities usually occurs when the crystalline solid cannot undergo a phase transition to a HP crystalline phase at a smaller pressure than that of amorphization. The hindrance of the pressure-driven phase transition between two crystalline phases is usually due to the presence of kinetic barriers between the low- and high-pressure structures. This barrier cannot be overcome if the temperature is not high enough and consequently the transition is frustrated at low temperatures. Therefore, it is worth to investigate which could be the frustrated HP phase of Tl$_2$O$_3$ and at which pressure the phase transition is predicted to occur.

In order to look for candidates of HP phases of Tl$_2$O$_3$, we have performed total-energy calculations for Tl$_2$O$_3$ with the structures observed experimentally in In$_2$O$_3$ at different pressures and temperatures. They include bixbyite-type (1a–3), corundum-type (S.G.: $R–3c$, No. 167, $Z = 6$), orthorhombic Rh$_2$O$_3$–II-type (S.G.: $Pbnm$, No. 60, $Z = 4$), and orthorhombic $z$-Gd$_2$S$_3$–type (S.G.: $Pnma$, No. 62, $Z = 4$) structures. We have also considered in our calculations the orthorhombic Rh$_2$O$_3$–III-type structure (S.G. $Pbca$, No. 61, $Z = 8$), which is a high-temperature and low-pressure form of Rh$_2$O$_3$, and two of the structures commonly found in rare-earth sesquioxides (RES) under different pressure and temperature conditions, like the monoclinic B-RES (S.G.: $C2/m$, No. 12, $Z = 6$) and trigonal A-RES (S.G.
$P - 3m1$, No. 164, $Z = 1$) structures. Finally, to complete the study, we have also considered as candidates for HP phases of $\text{Tl}_2\text{O}_3$ structures observed in transition-metal sesquioxides at different pressures and temperatures. These structures are the $\text{Sb}_2\text{S}_3$-type (S.G.: $Pnma$, No. 62, $Z = 4$) found in $\text{Tl}_2\text{O}_3$,$^{59,60}$ the distorted orthorhombic perovskite or $\text{GdFeO}_3$-type (S.G.: $Pnma$, No. 62, $Z = 4$) found in $\text{Fe}_2\text{O}_3$ (hematite),$^{61}$ and the orthorhombic post-perovskite or $\text{CaIrO}_2$-type (S.G.: $Cmcm$, No. 63, $Z = 4$) found in $\text{Mn}_2\text{O}_3$. $^{62}$

The enthalpy difference vs. pressure diagram for the different $\text{Tl}_2\text{O}_3$ polymorphs, taking as reference the enthalpy of the bixbyite-type phase, is plotted in Fig. 4. Our calculations predict a phase transition from the bixbyite-type phase ($Ia-3$) to the $\text{Rh}_2\text{O}_3$-II-type phase ($Pbcn$) at 5.8 GPa, and from the $\text{Rh}_2\text{O}_3$-II-type phase to the $\alpha$-$\text{Gd}_2\text{S}_3$-type phase ($Pnma$) at 24.2 GPa. This sequence of pressure-induced phase transitions for $\text{Tl}_2\text{O}_3$ is the same as for $\text{In}_2\text{O}_3$. $^{48,49}$ The main difference is the phase transition pressures predicted theoretically in both compounds: 5.8 GPa ($7–11$ GPa) and 24.2 GPa ($36–40$ GPa) for $\text{Tl}_2\text{O}_3$ ($\text{In}_2\text{O}_3$). $^{48,49}$ Those works already showed that large kinetic barriers are present in $\text{In}_2\text{O}_3$ at room temperature between the bixbyite-type, $\text{Rh}_2\text{O}_3$-II-type and $\alpha$-$\text{Gd}_2\text{S}_3$-type structures; therefore, similar barriers are expected to occur for the same structures in $\text{Tl}_2\text{O}_3$. In particular, the hypothesis of the kinetic frustration of the pressure-induced phase transition from the bixbyite-type to the $\text{Rh}_2\text{O}_3$-II-type structure in $\text{Tl}_2\text{O}_3$ will be explored in detail in future simultaneous HP and high temperature experiments on $\text{Tl}_2\text{O}_3$, as it was already done for $\text{In}_2\text{O}_3$. $^{48–52}$

C. Elastic properties

In order to further understand the amorphization process in $\text{Tl}_2\text{O}_3$, we have studied the mechanical stability of the cubic bixbyite-type ($Ia-3$) structure of $\text{Tl}_2\text{O}_3$ at HP. This structure belongs to the cubic Laue group $\text{CII}$ with point group $m-3$ which has three independent second order elastic constants: $C_{11}$, $C_{12}$, and $C_{44}$. Table III summarizes the values of the three $C_{ij}$ in $\text{Tl}_2\text{O}_3$ at zero pressure as obtained from our $ab\text{ initio}$ calculations. The calculated elastic constants of bixbyite-type $\text{In}_2\text{O}_3$ taken from Ref. 63 are also included in Table III for comparison. The values of the three elastic constants of $\text{Tl}_2\text{O}_3$ are smaller than those of $\text{In}_2\text{O}_3$. This result supports the smaller zero pressure bulk modulus of $\text{Tl}_2\text{O}_3$ when compared to that of $\text{In}_2\text{O}_3$ as previously commented.

A lattice is mechanically stable at zero pressure only if the Born stability criteria are fulfilled. $^{64}$ In the case of cubic systems, these criteria are

$$C_{11} + 2C_{12} > 0, C_{11} - C_{12} > 0, C_{44} > 0.$$  

TABLE III. Calculated $C_{ij}$ elastic constants and elastic moduli $B$, $G$, $E$ (in GPa) and the Poisson’s ratio, $\nu$, for $\text{Tl}_2\text{O}_3$ at zero pressure. Elastic moduli and Possion’s ratio are given in the Voigt, Reuss and Hill approximations, labeled respectively with subscripts $V$, $R$, and $H$. The $B/G$ ratio and the Zener anisotropy factor, $A$, are also given. Calculated data at zero pressure taken from Ref. 63 for $\text{In}_2\text{O}_3$ are also added for comparison.

<table>
<thead>
<tr>
<th></th>
<th>$\text{Tl}_2\text{O}_3$</th>
<th>$\text{In}_2\text{O}_3$</th>
</tr>
</thead>
<tbody>
<tr>
<td>$C_{11}$</td>
<td>177.0</td>
<td>234.3</td>
</tr>
<tr>
<td>$C_{12}$</td>
<td>99.2</td>
<td>107.2</td>
</tr>
<tr>
<td>$C_{44}$</td>
<td>32.8</td>
<td>62.7</td>
</tr>
<tr>
<td>$B = B_R = B_H$</td>
<td>125.1</td>
<td>149.6</td>
</tr>
<tr>
<td>$G_{V} = G_{R} = G_{H}$</td>
<td>35.3, 35.0, 35.1</td>
<td>63.0$^c$</td>
</tr>
<tr>
<td>$E_{V} = E_{R} = E_{H}$</td>
<td>96.7, 96.1, 96.4</td>
<td>165.8$^c$</td>
</tr>
<tr>
<td>$\nu_{V} = \nu_{R} = \nu_{H}$</td>
<td>0.37, 0.37, 0.37</td>
<td>0.32$^c$</td>
</tr>
<tr>
<td>$B_{V}/G_{V}, B_{R}/G_{R}, B_{H}/G_{H}$</td>
<td>3.55, 3.57, 3.56</td>
<td>2.37$^c$</td>
</tr>
<tr>
<td>$A$</td>
<td>0.84</td>
<td>0.99</td>
</tr>
</tbody>
</table>

$^a$ Our calculations with GGA-PBEsol prescription.

$^b$ Calculated with the GGA approximation.

$^c$ Results calculated in the Hill approximation from reported elastic constants.
In our particular case, all the above criteria are satisfied for bixbyite-type Tl\textsubscript{2}O\textsubscript{3} at zero pressure; therefore, cubic Tl\textsubscript{2}O\textsubscript{3} is mechanically stable at 1 atm (10\textsuperscript{-5} GPa), as it was expected. When a non-zero uniform stress is applied to the crystal, the above criteria to describe the stability limits of the crystal at finite strain are not adequate and the Born stability criteria must be modified. In this case, the elastic stiffness (or stress-strain) coefficients are defined as

\[ B_{ijkl} = C_{ijkl} + 1/2 [\delta_{ik}\sigma_{jl} + \delta_{jk}\sigma_{il} + \delta_{il}\sigma_{jk} + \delta_{jl}\sigma_{ik} - 2\delta_{ik}\delta_{jl}], \]  

(2)

where the \( C_{ijkl} \) are the elastic constants evaluated at the current stressed state, \( \sigma_{ij} \) correspond to the external stresses, and \( \delta_{ik} \) is the Kronecker delta.\textsuperscript{65–67} In the special case of hydrostatic pressure applied to a cubic crystal, \( \sigma_{11} = \sigma_{22} = \sigma_{33} = -P \), and the elastic stiffness coefficients are: \( B_{11} = C_{111} - P, B_{12} = C_{112} + P, \) and \( B_{44} = C_{444} - P, \) where \( P \) is the hydrostatic pressure. Note that the \( B_{ij} \) and \( C_{ij} \) coefficients are equal at 0 GPa. When the \( B_{ij} \) elastic stiffness coefficients are used, all the relations of the theory of elasticity can be applied including Born’s stability conditions which are identical in both loaded and unloaded states.\textsuperscript{66–69}

The bulk (\( B \)) and shear (\( G \)) moduli of cubic Tl\textsubscript{2}O\textsubscript{3} can be obtained in the Voigt,\textsuperscript{70} Reuss,\textsuperscript{71} and Hill\textsuperscript{72} approximations, labeled with subscripts \( V \), \( R \), and \( H \), respectively, using the formulae\textsuperscript{73}

\[ B_V = B_R = \frac{B_{11} + 2B_{12}}{3}, \]  

(3)

\[ B_H = \frac{B_V + B_R}{2}, \]  

(4)

\[ G_V = \frac{B_{11} - B_{12} + 3B_{44}}{5}, \]  

(5)

\[ G_R = \frac{5(B_{11} - B_{12})B_{44}}{4B_{44} + 3(B_{11} - B_{12})}. \]  

(6)

\[ G_H = \frac{G_V + G_R}{2}. \]  

(7)

In the Voigt (Reuss) approximation, uniform strain (stress) is assumed throughout the polycrystal.\textsuperscript{70,71} On the other hand, Hill has shown that the Voigt and Reuss averages are limits and suggested that the actual effective \( B \) and \( G \) elastic moduli can be approximated by the arithmetic mean of the two bounds.\textsuperscript{72} The Young (\( E \)) modulus and the Poisson’s ratio (\( \nu \)) are given by\textsuperscript{74,75}

\[ E_X = \frac{9B_XG_X}{G_X + 3B_X}, \]  

(8)

\[ \nu_X = \frac{1}{2}\left(\frac{3B_X - 2G_X}{3B_X + G_X}\right), \]  

(9)

where the subscript \( X \) refers to the symbols \( V, R, \) and \( H \). We summarize in Table III all the values obtained for \( B, G, E, \) and \( \nu \) in bixbyite-type Tl\textsubscript{2}O\textsubscript{3} at zero pressure in the Voigt, Reuss, and Hill approximations. Note that our calculated value for the bulk modulus in the Hill approximation (\( B_H = 125.1 \) GPa) is in very good agreement with the value of \( B_0 = 125.0(4) \) GPa obtained from our PBEsol structural calculations via a BM3 EOS fit. This result gives us confidence about the correctness of our elastic constants calculations.

Table III also includes the values of the ratio between the bulk and shear modulus, \( B/G \), and the Zener anisotropy factor, \( A \). The \( B/G \) ratio has been proposed by Pugh to predict brittle or ductile behavior of materials.\textsuperscript{76} According to the Pugh criterion, a \( B/G \) value above 1.75 indicates a tendency for ductility; otherwise, the material behaves in a brittle manner. In our particular case, we found a value of \( B/G = 3.56 \) in the Hill approximation indicating that the material should be ductile at 1 atm. The Zener anisotropy factor \( A \) for our cubic cell is defined as \( A = 2B_{44}/(B_{11} - B_{12}) \). If \( A \) is equal to one, no anisotropy exists. On the other hand, the

![FIG. 5. Pressure dependence of the theoretical (a) \( C_{ij} \) elastic constants and (b) \( B_{ij} \) elastic stiffness coefficients of bixbyite-type Tl\textsubscript{2}O\textsubscript{3}. Solid lines connecting the calculated data points are shown as a guide to the eyes.](image-url)
more this parameter differs from one, the more elastically anisotropic is the crystalline structure. In cubic $\text{Tl}_2\text{O}_3$, the $A$ value (0.84) is slightly different from 1 and evidence a small elastic anisotropy of our cubic cell at 1 atm.

Figures 5(a) and 5(b) show the pressure dependence of the three calculated $C_{ij}$ elastic constants and the three $B_{ij}$ elastic stiffness coefficients of bixbyite-type $\text{Tl}_2\text{O}_3$, respectively. It can be seen that $B_{11}$ and $B_{12}$ increase monotonically as pressure increases, while $B_{44}$ decreases monotonically as pressure increases and at 23.5 GPa crosses the 0 GPa horizontal line. This fact is related with the mechanical instability of bixbyite-type $\text{Tl}_2\text{O}_3$ and will be discussed in the next paragraphs.

The knowledge of the behavior of the three elastic stiffness coefficients with pressure allows us to study the mechanical stability of bixbyite-type $\text{Tl}_2\text{O}_3$ as pressure increases. The new conditions for elastic stability at a given pressure $P$, known as the generalized stability criteria, are obtained by replacing in Eq. (1) the $C_{ij}$ elastic constants by the $B_{ij}$ elastic stiffness coefficients, and are given by

\begin{equation}
M_1 = B_{11} + 2B_{12} > 0,
\end{equation}

\begin{equation}
M_2 = B_{11} - B_{12} > 0,
\end{equation}

\begin{equation}
M_3 = B_{44} > 0,
\end{equation}

where $B_{11}$, $B_{12}$, and $B_{44}$ are the elastic stiffness coefficients at the considered pressure. These generalized stability criteria are plotted in Fig. 6. It is found that Eq. (12), related to a pure shear instability, is violated at 23.5 GPa while Eq. (11), called the Born instability, is violated at 26.0 GPa. Therefore, our theoretical study of the mechanical stability of $\text{Tl}_2\text{O}_3$ at HP suggests that the bixbyite-type phase becomes mechanically unstable beyond 23.5 GPa. This pressure is slightly above but very close to the pressure at which the onset of PIA takes place experimentally. Consequently, this result suggests that shear instability could be involved in the PIA process of $\text{Tl}_2\text{O}_3$ at room temperature. We want to stress that our calculations are performed for a perfect
material, whereas our powder samples are very defective and contain a high concentration of O vacancies that make Tl₂O₃ a degenerate n-type semiconductor. Therefore, we expect that PIA in our sample takes place at a lower pressure than that theoretically predicted since defects are known to induce amorphization and decrease the pressure at which PIA begins in a number of materials. 

We have also performed the study of the dynamical stability in Tl₂O₃ in order to complement the study of the mechanical stability of Tl₂O₃ and verify that PIA in Tl₂O₃ is caused by the mechanical instability of the cubic phase. To check the dynamical stability of the cubic phase, we have carried out ab initio calculations of the phonon dispersion relations in bixbyite-type Tl₂O₃. We have found that the cubic phase is dynamically stable up to 32 GPa and that phonons with imaginary frequencies appear above this pressure. This result thus indicates that bixbyite-type Tl₂O₃ becomes dynamically unstable above 32 GPa. Since this pressure is higher than the pressure at which bixbyite-type Tl₂O₃ becomes dynamically unstable above 32 GPa, it is found that PIA of Tl₂O₃ observed at room temperature at 22 GPa might be caused by the mechanical instability of the cubic lattice at pressures above 22 GPa.

Finally, for completeness we have plotted the pressure dependence of the elastic moduli (BHH, GHH, and EHH), Poisson’s ratio, BHH/GHH ratio, and A Zener anisotropy factor in Fig. 7. It is found that BHH increases with pressure and reaches the value of 216.0 GPa at 23 GPa. On the other hand, GHH and EHH decrease with pressure approaching a value of 0 GPa near 23.5 GPa, pressure at which the mechanical instability is predicted to occur. We note that the fact that the shear modulus decreases with pressure is compatible with the fact that the equation that first is violated (Eq. (12)) is the one related with the pure shear instability because of the decreasing of BHH with pressure. The Poisson’s ratio, νHH, increases with pressure and reaches a value of 0.49 at 23 GPa. The BHH/GHH ratio increases with pressure, grows exponentially above 19 GPa, and reaches a value of 94.4 at 23 GPa. The increase of the BHH/GHH ratio with pressure indicates that the ductility of Tl₂O₃ is enhanced under compression. In the case of the Zener anisotropy factor, A, it is found that it increases with pressure reaching a maximum value of A = 0.96 at about 11 GPa and afterward decreases quickly above 20 GPa indicating a strong increase of the elastic anisotropy above that pressure.

V. CONCLUDING REMARKS

We have studied both experimentally and theoretically the structural properties of Tl₂O₃ under compression at room temperature. The equation of state of Tl₂O₃ has been determined and its bulk modulus has been found to be smaller than that of isostructural In₂O₃. Tl₂O₃ starts to amorphize above 22 GPa and retains the amorphous structure at 1 atm when decreasing pressure from 37.7 GPa. The theoretically predicted transitions to the Rh₂O₃-II-type structure, near 6 GPa, and to the z-Gd₂S₃-type structure, near 24 GPa, are not observed experimentally, probably, due to the kinetic hindrance of the phase transitions at room temperature.

To understand the pressure-induced amorphization process of Tl₂O₃, we have studied theoretically both the mechanical and dynamical stability of the cubic phase at high pressures. In this respect, the mechanical properties of bixbyite-type Tl₂O₃ at high pressures have been commented. Our calculations show that amorphization might be caused by the mechanical instability of the bixbyite-type structure predicted above 23.5 GPa since this phase is dynamically stable up to 32 GPa.

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