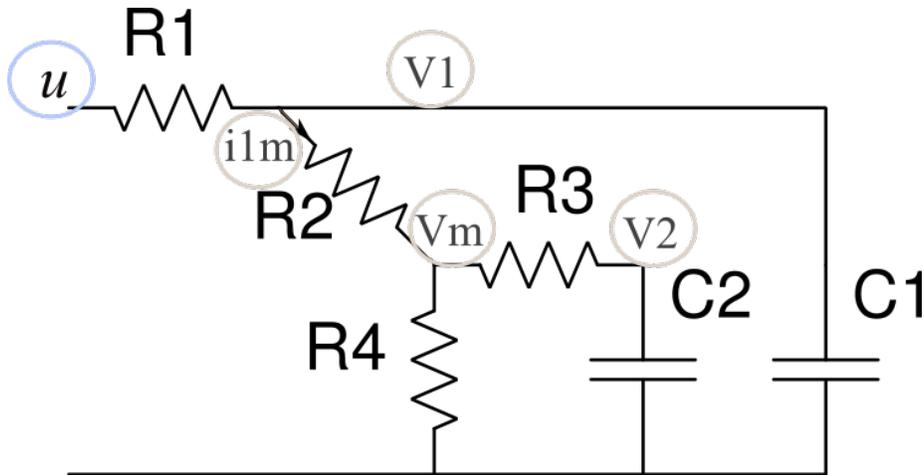


# Modelado de un circuito eléctrico (LFT) con DOS parámetros físicos inciertos.

© 2023, Antonio Sala Piqueras. Universitat Politècnica de València. Todos los derechos reservados.

Vídeo-presentación en <https://youtu.be/jDPdPuJyeA0>



Parámetros nominales:

```
C1_0=1e-3;C2=2e-3; R1=8;R3=16; R4=32; R2_0=4;
syms dv1 dv2 V1 V2 incR2 incC1 Vm u ilm
```

## standard model

La resistencia "real" R2 es R2\_0+incR2, el condensador "real" es C1\_0+incC1 modelo es:

```
R2=R2_0+incR2;C1=C1_0+incC1;
Model1=[C1*dv1==(u-V1)/R1-ilm; ...
C2*dv2==(Vm-V2)/R3; ...
ilm==(Vm-V2)/R3+Vm/R4; (V1-Vm)==R2*ilm ]
```

Model1 =

$$\begin{pmatrix} dv_1 \left( incC_1 + \frac{1}{1000} \right) = \frac{u}{8} - ilm - \frac{V_1}{8} \\ \frac{dv_2}{500} = \frac{V_m}{16} - \frac{V_2}{16} \\ ilm = \frac{3V_m}{32} - \frac{V_2}{16} \\ V_1 - V_m = ilm (incR_2 + 4) \end{pmatrix}$$

```
Unknowns=[dv1, ilm, Vm, dv2]; %remaining V1,V2,incR2,u
SolvedModel=solve (Model1,Unknowns)
```

SolvedModel = struct with fields:

```

dv1: (125*(16*V2 - 68*V1 + 44*u - 3*V1*incR2 + 3*incR2*u))/((3*incR2 + 44)*(1000*incC1 + 1))
ilm: (3*V1 - 2*V2)/(3*incR2 + 44)
Vm: (2*(16*V1 + 4*V2 + V2*incR2))/(3*incR2 + 44)
dv2: -(125*(36*V2 - 32*V1 + V2*incR2))/(4*(3*incR2 + 44))

```

```
StateEqs=simplify([SolvedModel.dv1; SolvedModel.dv2])
```

```
StateEqs =
```

$$\begin{pmatrix} \frac{125 (16 V_2 - 68 V_1 + 44 u - 3 V_1 \text{incR}_2 + 3 \text{incR}_2 u)}{(3 \text{incR}_2 + 44) (1000 \text{incC}_1 + 1)} \\ -\frac{125 (36 V_2 - 32 V_1 + V_2 \text{incR}_2)}{4 (3 \text{incR}_2 + 44)} \end{pmatrix}$$

```
A=jacobian(StateEqs, [V1, V2])
```

```
A =
```

$$\begin{pmatrix} -\frac{125 (3 \text{incR}_2 + 68)}{(3 \text{incR}_2 + 44) (1000 \text{incC}_1 + 1)} & \frac{2000}{(3 \text{incR}_2 + 44) (1000 \text{incC}_1 + 1)} \\ \frac{1000}{3 \text{incR}_2 + 44} & -\frac{125 (\text{incR}_2 + 36)}{4 (3 \text{incR}_2 + 44)} \end{pmatrix}$$

```
B=jacobian(StateEqs, [u])
```

```
B =
```

$$\begin{pmatrix} \frac{125}{1000 \text{incC}_1 + 1} \\ 0 \end{pmatrix}$$

Introduzcamos ecuación de salida... por ejemplo, se dispone de sensor/objetivos de control en V1 y Vm

```
OutputEqs=[V1; SolvedModel.Vm];
C=jacobian(OutputEqs, [V1 V2])
```

```
C =
```

$$\begin{pmatrix} 1 & 0 \\ \frac{32}{3 \text{incR}_2 + 44} & \frac{2 (\text{incR}_2 + 4)}{3 \text{incR}_2 + 44} \end{pmatrix}$$

```
D=jacobian(OutputEqs, [u])
```

```
D =
```

$$\begin{pmatrix} 0 \\ 0 \end{pmatrix}$$

El modelo "nominal" sería:

```
incR2=0; incC1=0;
Anum=eval(A)
```

```
Anum = 2x2
-193.1818    45.4545
```

22.7273 -25.5682

```
Bnum=eval(B)
```

```
Bnum = 2x1
    125
     0
```

```
Cnum=eval(C)
```

```
Cnum = 2x2
    1.0000     0
    0.7273    0.1818
```

```
Dnum=eval(D)
```

```
Dnum = 2x1
     0
     0
```

```
circuitnominal=ss(Anum,Bnum,Cnum,Dnum);
```

## introducing changes in the model to incorporate LFT

Redeclaremos `incr2` como simbólica (borremos su valor de cero de antes), y introduzcamoslo en forma LFT

```
syms incr2 incC1 w_deltaR w_deltaC Ana %extra symbolic variables
Model_sinR2C1=[ dv1==Ana; ...
    C2*dv2==(Vm-V2)/R3; ...
    ilm==(Vm-V2)/R3+Vm/R4;];
EqResistor2_LFT= ( (V1-Vm)==R2_0*ilm+w_deltaR );
EqC1_LFT= ( C1_0*Ana+w_deltaC==(u-V1)/R1-ilm );
Eq_Uncertainty = [w_deltaR==incr2*ilm; w_deltaC==incC1*Ana];
```

La parte lineal "cierta" del modelo es esta:

```
Model2=[Model_sinR2C1; EqResistor2_LFT; EqC1_LFT]
```

Model2 =

$$\begin{pmatrix} dv_1 = Ana \\ \frac{dv_2}{500} = \frac{V_m}{16} - \frac{V_2}{16} \\ ilm = \frac{3V_m}{32} - \frac{V_2}{16} \\ V_1 - V_m = 4ilm + w_{\text{delta}R} \\ \frac{Ana}{1000} + w_{\text{delta}C} = \frac{u}{8} - ilm - \frac{V_1}{8} \end{pmatrix}$$

El modelo nominal será  $w_{\text{delta}R}=w_{\text{delta}C}=0$ .

El modelo completo será (equiv. a Model 1):

```
Model3=[Model2; Eq_Uncertainty]
```

```
Model3 =
```

$$\begin{pmatrix} dv_1 = Ana \\ \frac{dv_2}{500} = \frac{V_m}{16} - \frac{V_2}{16} \\ i_{lm} = \frac{3 V_m}{32} - \frac{V_2}{16} \\ V_1 - V_m = 4 i_{lm} + w_{\Delta R} \\ \frac{Ana}{1000} + w_{\Delta C} = \frac{u}{8} - i_{lm} - \frac{V_1}{8} \\ w_{\Delta R} = i_{lm} incR_2 \\ w_{\Delta C} = Ana incC_1 \end{pmatrix}$$

```
Unknowns3=[Unknowns w_deltaR w_deltaC Ana ];
SolvedModel3=solve(Model3, Unknowns3)
```

```
SolvedModel3 = struct with fields:
```

```
dv1: (125*(16*V2 - 68*V1 + 44*u - 3*V1*incR2 + 3*incR2*u))/(44000*incC1 + 3*incR2 + 3000*incC1*incR2)
i1m: (3*V1 - 2*V2)/(3*incR2 + 44)
Vm: (2*(16*V1 + 4*V2 + V2*incR2))/(3*incR2 + 44)
dv2: -(125*(36*V2 - 32*V1 + V2*incR2))/(4*(3*incR2 + 44))
w_deltaR: (3*V1*incR2 - 2*V2*incR2)/(3*incR2 + 44)
w_deltaC: (125*incC1*(16*V2 - 68*V1 + 44*u - 3*V1*incR2 + 3*incR2*u))/(44000*incC1 + 3*incR2 + 3000*incC1*incR2)
Ana: (125*(16*V2 - 68*V1 + 44*u - 3*V1*incR2 + 3*incR2*u))/(44000*incC1 + 3*incR2 + 3000*incC1*incR2)
```

Que resulta, en tanto a  $dv_1$ ,  $dv_2$ ,  $i_{lm}$ ,  $V_m$ , exactamente igual que el Model1. Comprobemos, por ejemplo A

```
LaMismaA=simplify(jacobian([SolvedModel3.dv1, SolvedModel3.dv2],[V1 V2]))
```

```
LaMismaA =
```

$$\begin{pmatrix} -\frac{125(3 incR_2 + 68)}{(3 incR_2 + 44)(1000 incC_1 + 1)} & \frac{2000}{(3 incR_2 + 44)(1000 incC_1 + 1)} \\ \frac{1000}{3 incR_2 + 44} & -\frac{125(incR_2 + 36)}{4(3 incR_2 + 44)} \end{pmatrix}$$

```
A-LaMismaA
```

```
ans =
```

$$\begin{pmatrix} 0 & 0 \\ 0 & 0 \end{pmatrix}$$

**Modelado LFT: NO usar Eq\_Uncertainty, con lo que w\_delta es una entrada "virtual"**

```
SolvedModelLFT=solve(Model2, [Unknowns Ana])
```

```
SolvedModelLFT = struct with fields:
```

```
dv1: (500*V2)/11 - (2125*V1)/11 + 125*u - 1000*w_deltaC + (750*w_deltaR)/11
i1m: (3*V1)/44 - V2/22 - (3*w_deltaR)/44
Vm: (8*V1)/11 + (2*V2)/11 - (8*w_deltaR)/11
```

$$\begin{aligned} dv2: & (250*V1)/11 - (1125*V2)/44 - (250*w\_deltaR)/11 \\ Ana: & (500*V2)/11 - (2125*V1)/11 + 125*u - 1000*w\_deltaC + (750*w\_deltaR)/11 \end{aligned}$$

El resultado, claro, depende de  $w\_deltaR$  y  $w\_deltaC$

```
StateEqsLFTModel=[SolvedModelLFT.dv1;SolvedModelLFT.dv2]
```

StateEqsLFTModel =

$$\begin{pmatrix} \frac{500 V_2}{11} - \frac{2125 V_1}{11} + 125 u - 1000 w_{\text{delta}C} + \frac{750 w_{\text{delta}R}}{11} \\ \frac{250 V_1}{11} - \frac{1125 V_2}{44} - \frac{250 w_{\text{delta}R}}{11} \end{pmatrix}$$

Representación interna completa como upper LFT

```
A=jacobian(StateEqsLFTModel,[V1,V2])
```

A =

$$\begin{pmatrix} -\frac{2125}{11} & \frac{500}{11} \\ \frac{250}{11} & -\frac{1125}{44} \end{pmatrix}$$

```
GeneralisedInput=[w_deltaR, w_deltaC, u];
B_lft=jacobian(StateEqsLFTModel, GeneralisedInput)
```

B\_lft =

$$\begin{pmatrix} \frac{750}{11} & -1000 & 125 \\ -\frac{250}{11} & 0 & 0 \end{pmatrix}$$

```
GeneralisedOutputEq=[SolvedModelLFT.i1m;SolvedModelLFT.Ana;V1;SolvedModelLFT.Vm]; %añadido
C_lft=jacobian(GeneralisedOutputEq,[V1,V2])
```

C\_lft =

$$\begin{pmatrix} \frac{3}{44} & -\frac{1}{22} \\ -\frac{2125}{11} & \frac{500}{11} \\ 1 & 0 \\ \frac{8}{11} & \frac{2}{11} \end{pmatrix}$$

```
D_lft=jacobian(GeneralisedOutputEq,GeneralisedInput)
```

D\_lft =

$$\begin{pmatrix} -\frac{3}{44} & 0 & 0 \\ \frac{750}{11} & -1000 & 125 \\ 0 & 0 & 0 \\ -\frac{8}{11} & 0 & 0 \end{pmatrix}$$

Comprobemos que la interconexión LFT da el resultado correcto (modelo original):

```
incR2=0; incC1=0;
sysuncert=diag([incR2;incC1]);
sys2=ss(eval(A),eval(B_lft),eval(C_lft),eval(D_lft));
circuito_otra_vez=lft(sysuncert,sys2);
norm(circuito_otra_vez-circuitnominal,'inf')
```

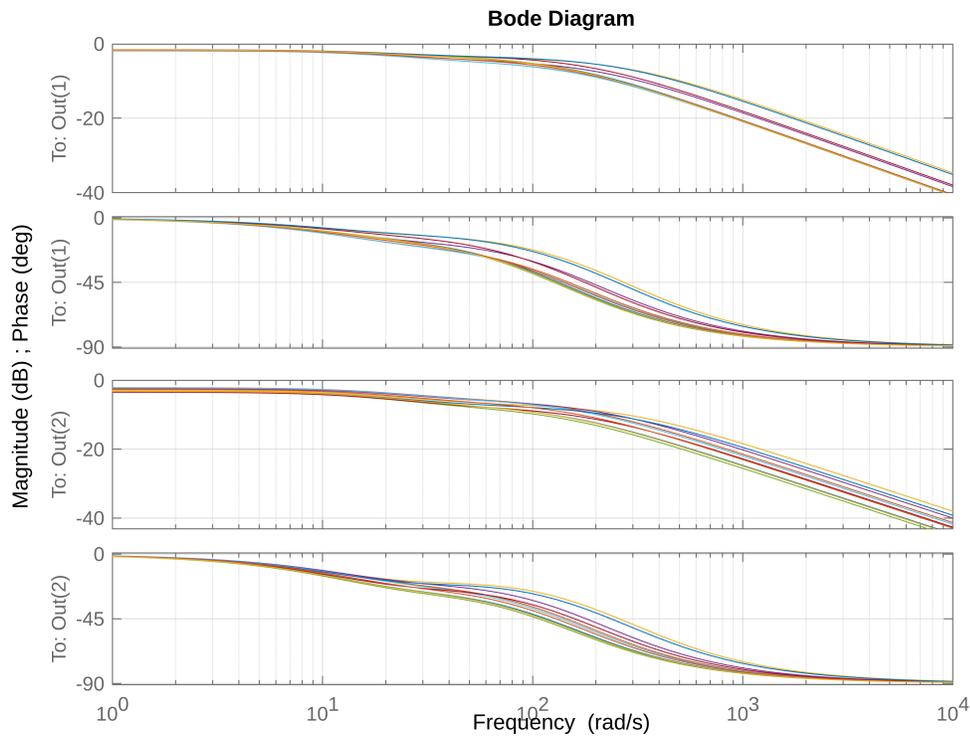
```
ans = 2.7756e-17
```

Simulemos variaciones de resistencia y capacidades al azar:

```
for i=1:10
    incR2=8*(rand()-0.5); incC1=8e-4*(rand()-0.5);
    sysuncert=diag([incR2;incC1]);
    circmodif=lft(sysuncert,sys2);
    bode(circmodif)
    hold on
    [incR2 incC1*1e4 norm(circmodif-circuitnominal,'inf')]
end
```

```
ans = 1x3
    2.5178    3.2463    0.1334
ans = 1x3
   -2.9841    3.3070    0.1025
ans = 1x3
    1.0589   -3.2197    0.1437
ans = 1x3
   -1.7720    0.3751    0.0458
ans = 1x3
    3.6601    3.7191    0.1571
ans = 1x3
   -2.7391    3.7647    0.1107
ans = 1x3
    3.6573   -0.1170    0.0771
ans = 1x3
    2.4022   -2.8649    0.1211
ans = 1x3
   -0.6259    3.3259    0.1063
ans = 1x3
    2.3377    3.6759    0.1432
```

```
hold off, grid on
```



Márgen de estabilidad ante incertidumbre no estructurada (R2 no lineal, con retardo, dinámica...)

```
mgst=1/norm(sys2(1:2,1:2),'inf')
```

```
mgst = 9.9768e-04
```

El resultado da un margen "pequeño"... problema: se ha mezclado incR2 con incC1, tienen unidades distintas... Necesaria "ponderación" (normalización) para que los márgenes tengan significado, mgst no se sabe las unidades que tiene.