Case study: actuator (manipulated variables) and controlled variable selection, polyhedra vs SVD tools

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Presentations in video:

http://personales.upv.es/asala/YT/V/sacerf1EN.html

http://personales.upv.es/asala/YT/V/sacerf2EN.html

http://personales.upv.es/asala/YT/V/sacerf3EN.html

http://personales.upv.es/asala/YT/V/sacerf4EN.html

http://personales.upv.es/asala/YT/V/sacerf5EN.html

http://personales.upv.es/asala/YT/V/sacerf6EN.html

http://personales.upv.es/asala/YT/V/sacerf7EN.html

This code runs in Matlab R2023a (Linux)

Objectives: understand SVD and polyhedron geometry and manipulations to asses wheter given setpoint increments or worst-case disturbance rejection are feasible without saturation.

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Model and constraints

Consider a linearised model $y_{2\times 1} = G_{2\times 3}u_{3\times 1} + H_{2\times 2}d_{2\times 1}$ with an operating point given by:

```
y_eq=[9 1.45]; u_eq=[2 0.5 1.7]; d_eq=[3 2];
```

where G and H are the transfer function matrices:

```
 s=tf('s'); \\ G=[3/(s+2) \quad 0.15/(2*s+1) \quad -9/(0.3*s+1); \\ 0.15/(0.5*s+1) \quad -0.2/(s+1) \quad 1.9/(0.3*s+1)]; \\ H=[1.8/(s+1)^2 \quad 2/(s+3); \quad 2.4/(s+12) \quad 0.6/(s+1)/(s+3)];
```

Later on, we'll see that we can achieve all that we are required to... Hence, if we wish to test "actuator selection", using just two of them, we may make some columns of G equal to zero and execute the code again:

```
G=G*diag([1 1 1]); %set to zero position of actuator to disable.
```

Of course, "elliminating" one actuator should be, in rigor, "deleting" the column, but that would change the size of matrices so code would give errors. Setting column to zero is a quick workaround.

Manipulated variables u have the following saturation limits:

```
lim_u_abs=[4 1.5 2; 0 0 1]; %1st row max, 2nd row min
```

In incremental units, the limits of manipulated variables are:

A) Reference tracking in steady state without saturation, SVD geometry

Basic computations

We wish to be able to move the outputs (via setpoint changes to be tracked by controllers) in the ranges:

```
lim_y_abs=[11.6 1.6; 8.5 1.35]; %1st row max, 2nd row min
```

So, in incremental units, these desired increments are:

```
inc_y_desired=lim_y_abs-y_eq
```

```
inc_y_desired = 2x2
2.6000 0.1500
-0.5000 -0.1000
```

Static DC gain matrix is:

```
Gain=dcgain(G)
```

Scaling step: $y = E_y \cdot y_{esc}$, $u = E_u \cdot u_{esc}$

Ey=diag(max(abs(inc_y_desired))) %worst case is maximum desired output increment

$$Ey = 2x2$$
2.6000 0
0.1500

Eu=diag(min(abs(inc_u_admissible))) %worst case is minimum available input increment

The scaled gain matrix is given by:

$$y_{esc} = E_y^{-1} y = E_y^{-1} Gu = \underbrace{E_y^{-1} GE_u}_{scaled \ gain} \cdot u_{esc}$$

Gain scaled=inv(Ey)*Gain*Eu %Scaling for unit increments desired/available.

svd(Gain_scaled)

```
ans = 2x1
4.3646
1.4985
```

Minimum gain is almost 1.5, above 1: satisfactory. Condition number is:

ans = 2.9127

The value of around 3 is quite sensible, lower than 5.

Hence, the answer is YES: we can move the outputs to the required amplitudes (steady state) with available inputs, when considering the geometry of ellipses, i.e., achieving any y_{esc} such that $||y_{esc}|| = 1$ with $||u_{esc}|| \le 1$, norm is the Euclidean norm.

In a "pen-and-paper plus basic calculator" examination for my M.Sc. students this would finish the required answer.

Further discussion

We will now examine singular vectors (principal directions) for further insight:

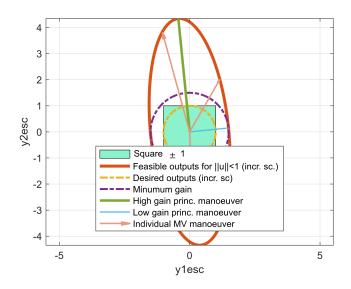
```
[U,S,V]=svd(Gain scaled)
U = 2 \times 2
   -0.0991
            0.9951
   0.9951
            0.0991
s = 2 \times 3
    4.3646
                    0
                               0
        Ω
              1.4985
                               0
V = 3 \times 3
    0.4298
             0.8985
                        0.0891
   -0.1526
             -0.0249
                         0.9880
    0.8899
             -0.4382
                         0.1264
```

Intuitively, the "hard" manoeuver is, roughly, increase 1 unit output 1 and increase 0.1 units output 2 (grosso modo, keep it where it was), being manipulated variable 1 the most critical.

Also, as minimum gain is above $\sqrt{2}$, then the "unit sphere in u" will be able to achieve all output manoeuvers in the sphere of radius 1.49 in y space, which of course will include the "unit square in y, vertices at ± 1 "; thus, the validity in the polyhedron geometry can be asserted without any polyhedron-specific code. This would not occur if the minimum gain were lower than $\sqrt{\text{num. outputs}}$. Let us graphically represent the above ideas.

If we draw the output ellipse swept by inputs $||u_{esc}|| = 1$ when multiplied by G_{esc} , we have:

```
plot([0 U(1,1)*S(1,1)],[0 U(2,1)*S(1,1)],LineWidth=2.5) %output direction 1, scaled
plot([0 U(1,2)*S(2,2)],[0 U(2,2)*S(2,2)],LineWidth=1.25) %output direction 2, scaled
for i=1:3
    quiver(0,0,Gain_scaled(1,i),Gain_scaled(2,i),0,Color=[.9 .6 .5],LineWidth=1.5);
end
hold off, axis equal
xlabel("ylesc"),ylabel("y2esc")
legend("Square \pm 1","Feasible outputs for ||u||<1 (incr. sc.)","Desired outputs (incr.</pre>
```



B) Steady state reference tracking, Polyhedron geometry

Basic computations

With polyhedron code, there is no need for "scaled" units, and in fact as ranges are quite asymmetric, even in scaled units the desired increments will not be "unity".

So, we'll work in original non-scaled units, but of course in INCREMENTAL ones, as we are working with a linear system. We have:

```
Vertices incy=[8.5 8.5 11.6 11.6;1.35 1.6 1.6 1.35]-[9;1.45] %desired extreme points
Vertices incy = 2x4
                     2.6000
  -0.5000 -0.5000
                             2.6000
  -0.1000
            0.1500
                     0.1500
                            -0.1000
Vertices incy=Vertices incy; %scaling to check for extra margin
Min incU=inc u admissible(2,:) %Lower Bound
Min incU = 1 \times 3
  -2.0000 -0.5000
                    -0.7000
Max incU=inc u admissible(1,:) %Upper Bound
Max incU = 1x3
   2.0000
            1.0000
                     0.3000
```

We must check if there is a feasible *u* for each of the four extreme vertices of desired output.

The code below minimises $||u||^2$ subject to Gan-u=vertex, and subject to u being inside the maximum and minimum increment bounds.

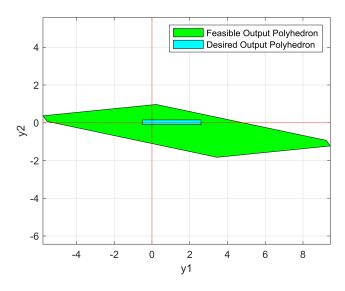
```
quadprog(inv(Eu)^2,zeros(1,3),[],[],Gain,Vertices incy(:,1),Min incU,Max incU) %factible
Minimum found that satisfies the constraints.
Optimization completed because the objective function is non-decreasing in
feasible directions, to within the value of the optimality tolerance,
and constraints are satisfied to within the value of the constraint tolerance.
<stopping criteria details>
ans = 3x1
   -0.4356
   0.0134
   -0.0168
quadprog(inv(Eu)^2,zeros(1,3),[],[],Gain,Vertices incy(:,2),Min incU,Max incU) % NO
Minimum found that satisfies the constraints.
Optimization completed because the objective function is non-decreasing in
feasible directions, to within the value of the optimality tolerance,
and constraints are satisfied to within the value of the constraint tolerance.
<stopping criteria details>
ans = 3 \times 1
   0.0891
   -0.0170
   0.0701
quadprog(inv(Eu)^2,zeros(1,3),[],[],Gain,Vertices incy(:,3),Min incU,Max incU) % NO fac
Minimum found that satisfies the constraints.
Optimization completed because the objective function is non-decreasing in
feasible directions, to within the value of the optimality tolerance,
and constraints are satisfied to within the value of the constraint tolerance.
<stopping criteria details>
ans = 3 \times 1
   1.4887
   -0.0248
   -0.0412
quadprog(inv(Eu)^2,zeros(1,3),[],[],Gain,Vertices incy(:,4),Min incU,Max incU) %factible
Minimum found that satisfies the constraints.
Optimization completed because the objective function is non-decreasing in
feasible directions, to within the value of the optimality tolerance,
and constraints are satisfied to within the value of the constraint tolerance.
<stopping criteria details>
ans = 3x1
   0.9639
    0.0056
```

As all vertices are feasible, we have proven that the requested steady state setpoint tracking problem is feasible without MV saturation, and we can achieve any point in the desired "output box". We knew it from the minimum-gain SVD computations, anyway.

Further discussion

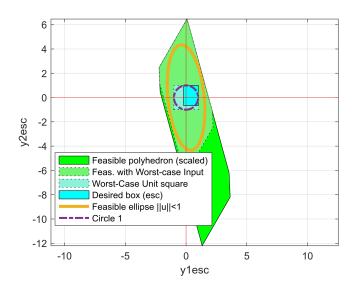
Let us graphically represent the result of the above computations.

```
inc u admissible
inc u admissible = 2 \times 3
   2.0000
           1.0000
                     0.3000
  -2.0000
           -0.5000
                   -0.7000
VerticesIncU=[2 1 .3;2 1 -.7;2 -.5 -.7;2 -.5 .3;-2 1 .3;-2 1 -.7;-2 -.5 -.7;-2 -.5
                                                                                            .3]
VerticesIncU = 3x8
   2.0000
           2.0000
                    2.0000
                             2.0000
                                       -2.0000
                                                -2.0000
                                                         -2.0000
                                                                  -2.0000
                                                                  -0.5000
                    -0.5000
                             -0.5000
                                                1.0000
                                                         -0.5000
   1.0000
           1.0000
                                       1.0000
   0.3000
           -0.7000
                    -0.7000
                              0.3000
                                       0.3000
                                                -0.7000
                                                         -0.7000
                                                                   0.3000
ImageVerticesU=Gain*VerticesIncU
ImageVerticesU = 2x8
   0.4500
           9.4500
                     9.2250
                              0.2250
                                       -5.5500
                                                 3.4500
                                                          3.2250
                                                                  -5.7750
                    -0.9300
                              0.9700
                                                -1.8300
                                                         -1.5300
                                                                   0.3700
   0.6700
           -1.2300
                                       0.0700
k=convhull(ImageVerticesU(1,:),ImageVerticesU(2,:)); %Order is important for "fill"
fill(ImageVerticesU(1,k),ImageVerticesU(2,k),'g') %feasible polyhedron
hold on
fill (Vertices incy(1,:), Vertices incy(2,:), 'c')
hold off, grid on, axis equal
xlabel("y1"), ylabel("y2")
xline(0,'r'), yline(0,'r'), legend("Feasible Output Polyhedron", "Desired Output Polyhedron"
```



Even if it is not strictly needed, we can plot in "scaled" units, to compare with the ellipses, etc:

```
VerticesIncU_SquareWorstCase=[2 .5 .3;2 .5 -.3;2 -.5 -.3;2 -.5 .3;-2 .5 .3;-2 .5 -.3;-2
ImageVerticesUWC=Gain*VerticesIncU_SquareWorstCase;
fill(1/Ey(1,1)*ImageVerticesU(1,k),1/Ey(2,2)*ImageVerticesU(2,k),'g'),
hold on
fill(1/Ey(1,1)*ImageVerticesUWC(1,k),1/Ey(2,2)*ImageVerticesUWC(2,k),[0.45 0.95 0.45],I
fill([-1 -1 1 1],[-1 1 1 -1],[0.55 0.95 0.85],LineStyle=':'), hold on %unit square
fill(1/Ey(1,1)*Vertices_incy(1,:),1/Ey(2,2)*Vertices_incy(2,:),'c'),
fimplicit(y'*inv(M)*y-1, LineWidth=3), grid on %feasible ellipse
fimplicit(y'*y-1, '-.',LineWidth=2) %unit circle
hold off, axis equal, xline(0,'r'),yline(0,'r')
xlabel("ylesc"),ylabel("y2esc")
legend("Feasible polyhedron (scaled)","Feas. with Worst-case Input","Worst-Case Unit scaled)
```



On scaling and relation to predictive control or LQR cost index

If we wished to achieve a given setpoint minimising $\|u\|$ in "online" operation, we would end up doing something VERY similar to the above quadprog. MPC would use not just the DC gain, but the whole step response (DMC). In a general case, if each element of u has its own units and range, we should actually minimise $\|u_{esc}\|^2$ so that all increments are "comparable". We may switch to G_{esc} and scale output accordingly, or we may keep original units and minimise $\|u_{esc}\|^2 = \|E_u^{-1}u\|^2$, from the fact that, by definition, $u = E_u u_{esc}$. This would just require to change the first argument to quadprog from "eye (3)" to "inv (E u) ^2".

C) Total disturbance rejection without saturation (steady state) SVD geometry

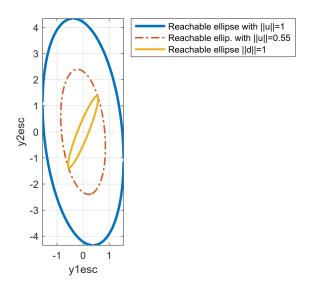
With a model y = Gu + Hd, input to fully cancel the effect of disturbance is disturbance multiplied by the "feedforward gain matrix" $-G^{-1}H$ o; in the case G is not square, we need pseudoinverse (scaled):

```
interv d=[3.8 2.4;2.4 1.35]; %range (absolute units) of the two disturbances.
operatingpoint d=[3 2];
incr d=interv d-operatingpoint d %incremental units
incr d = 2x2
  0.8000 0.4000
  -0.6000 -0.6500
Ed=diag(max(abs(incr d))) %worst case is maximum disturbance
Ed = 2 \times 2
   0.8000
           0.6500
Hgesc=inv(Ey)*dcgain(H)*Ed;
%Actually, Ey is not relevant for total cancellation. Only Eu and Ed matter.
FeedForward=-pinv(Gain scaled)*Hgesc
FeedForward = 3x2
  -0.4930 -0.2343
   0.0461
           0.0338
  -0.0131 -0.0989
u sv=svd(FeedForward)
u sv = 2x1
   0.5515
   0.0838
```

Maximum gain <1 means that scaled disturbances $||d_{esc}|| \le 1$ can be cancelled with $||u_{esc}|| \le 0.552 < 1$.

Graphical representation

```
Md=Hgesc*Hgesc';
fimplicit(y'*inv(M)*y-1, LineWidth=2.5), grid on %feasible ellipse
hold on
%elipsoide que las entradas pueden mover
fimplicit(y'*inv(M)*y-u_sv(1)^2, '-.',LineWidth=1.5), grid on %feasible ellipse
fimplicit(y'*inv(Md)*y-1, LineWidth=2) %output ellipse in open loop due to disturbances
xlabel("ylesc"),ylabel("y2esc")
hold off, axis equal, legend("Reachable ellipse with ||u||=1", "Reachable ellip. with |
```



Indeed, we can see that the effect of u is larger than that of d, so u has no problems to counteract the "yellow" ellipsoid producing an output contrary to it inside the "red" ellipsoid.

Polyhedron geometry, total cancellation (steady state)

```
%zoomfactor=1;
zoomfactor=2.08 %for partial rejection, later on

zoomfactor = 2.0800

%zoomfactor=1.78 %max. feasible for total rejection below
Vertices_incD=[0.8 0.8 -0.6 -.6; 0.4 -0.65 0.4 -0.65]*zoomfactor

Vertices_incD = 2x4
    1.6640    1.6640    -1.2480    -1.2480
    0.8320    -1.3520    0.8320    -1.3520

1/zoomfactor

ans = 0.4808
```

*Minimising $||u_{scaled}||^2 = u^T (E_u^{-1})^2 u$ would make pseudo-inverse results coincident with quadprog ones (if pseudo-inverse were feasible). Note, however, that actual "implementation" would need a feedforward (measurable disturbance) component, both here and in the pseudo-inverse SVD computations.

```
for i=1:4
    i
    quadprog(inv(Eu^2), zeros(1,3),[],[],Gain,-dcgain(H)*Vertices_incD(:,i),Min_incU,Max
end

i = 1
No feasible solution found.
```

quadprog stopped because it was unable to find a point that satisfies

the constraints within the value of the constraint tolerance.

```
<stopping criteria details>
i = 2
```

Minimum found that satisfies the constraints.

Optimization completed because the objective function is non-decreasing in feasible directions, to within the value of the optimality tolerance, and constraints are satisfied to within the value of the constraint tolerance.

<stopping criteria details>
i = 3

Minimum found that satisfies the constraints.

Optimization completed because the objective function is non-decreasing in feasible directions, to within the value of the optimality tolerance, and constraints are satisfied to within the value of the constraint tolerance.

<stopping criteria details>
i = 4
No feasible solution found.

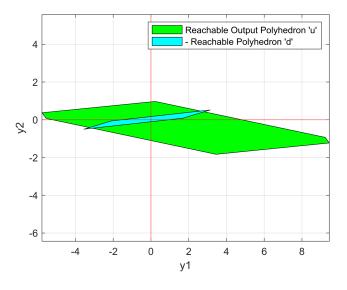
quadprog stopped because it was unable to find a point that satisfies the constraints within the value of the constraint tolerance.

<stopping criteria details>

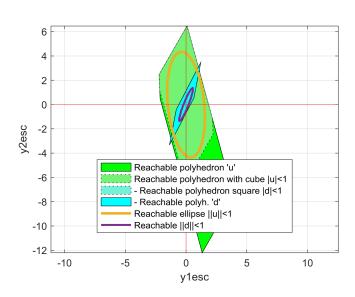
So, we may plot the relevant polyhedra to check the meaning of the above. In Non-scaled coordinates:

```
ImageVerticesd=-dcgain(H)*Vertices_incD; %Change sign, because "u" must counteract the
kd=convhull(ImageVerticesd(1,:),ImageVerticesd(2,:)); %Order is important for "fill"

fill(ImageVerticesU(1,k),ImageVerticesU(2,k),'g') %feasible polyhedron
hold on
fill(ImageVerticesd(1,kd),ImageVerticesd(2,kd),'c')
hold off, grid on, axis equal
xlabel("y1"),ylabel("y2")
xline(0,'r'),yline(0,'r'), legend("Reachable Output Polyhedron 'u'","- Reachable Polyhedron
```



Even if it is not strictly needed, we can plot in "scaled" output units, to compare with the ellipses, etc:



D) partial disturbance rejection (steady state)

D.1) Polyhedron geometry

Now, we change to $-\epsilon_{Low} \leq Gu + Hd \leq +\epsilon_{High}$ or, well, the bound we wish...

Rewrite first inequality as $-\epsilon_{Low} - Hd \le Gu$, $-Gu \le \epsilon_{Low} + Hd$ and second one as $Gu \le \epsilon_{High} - Hd$. Even the bound may be "vertex dependent" (left to the reader/viewer).

For instance, if we want residual error in [-.1, +.2] in y_1 and [-.15, +.25] in y_2 , for all vertex disturbances, we will check the feasibility of the inequalities with "quadprog".

As quadprog is an "optimization" algorithm minimising $\frac{1}{2}u^THu + f^Tu$, we might think on what to minimise; we have several options:

- minimising $||u_{scaled}||^2$ so that we exert the "minimum control effort" to keep the errors within bounds. In this case, $H = (E_u^{-1})^2$, f = 0.
- minimising $||y_{scaled}||^2$, so that we achieve zero output deviation, if feasible; otherwise, we minimise the residual deviation (weighted least squares with a technologically relevant output scaling). In this case:

$$\|G_{esc}u + H_{esc}d\|^2 = (G_{esc}u + H_{esc}d)^T \cdot (G_{esc}u + H_{esc}d) = u^T \cdot G_{esc}^T G_{esc} \cdot u + 2d^T H_{esc}^T G_{esc} \cdot u + d^T \cdot H_{esc}^T H_{esc} \cdot d$$

so, as d is not a decision variable, we would have

$$H = G_{esc}^T G_{esc}$$
 , $f = 2d^T H_{esc}^T G_{esc}$.

• Something in between, say, minimising $J = \|y_{scaled}\|^2 + \rho \cdot \|u_{scaled}\|^2$, so weight ρ is used to balance control effort usage versus output residual error magnitude.

However, as the cost index (in second and third cases) and constraints in quadprog depend on d, in principle, this would require a "feedforward" (measurable d) control structure: this would not be an issue in (known) setpoint tracking, but it is in rejection of unmeasurables disturbances. As we are just interested in "feasibility", not actual "predictive control implementation", we'll just use the first (simplest) option.

```
lim_elow=[.1;.15]; lim_ehigh=[+.2;+.25]; %we set whatever limits we wish...
for i=1:4
    i
    Aineq=[-Gain;
        Gain];
    Bineq=[lim_elow+dcgain(H)*Vertices_incD(:,i);
        lim_ehigh-dcgain(H)*Vertices_incD(:,i)];
    quadprog(inv(Eu^2),zeros(1,3),Aineq,Bineq,[],[],Min_incU,Max_incU);
end
```

```
i = 1
Minimum found that satisfies the constraints.

Optimization completed because the objective function is non-decreasing in feasible directions, to within the value of the optimality tolerance, and constraints are satisfied to within the value of the constraint tolerance.

<stopping criteria details>
i = 2
```

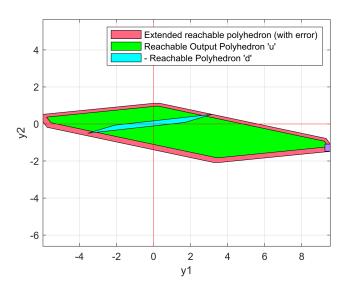
Minimum found that satisfies the constraints. Optimization completed because the objective function is non-decreasing in feasible directions, to within the value of the optimality tolerance, and constraints are satisfied to within the value of the constraint tolerance. <stopping criteria details> i = 3Minimum found that satisfies the constraints. Optimization completed because the objective function is non-decreasing in feasible directions, to within the value of the optimality tolerance, and constraints are satisfied to within the value of the constraint tolerance. <stopping criteria details> i = 4Minimum found that satisfies the constraints. Optimization completed because the objective function is non-decreasing in feasible directions, to within the value of the optimality tolerance, and constraints are satisfied to within the value of the constraint tolerance.

<stopping criteria details>

Of course, as perfect cancellation was feasible, so it is imperfect cancellation, this is just to learn how to do it.

We can zoom out disturbance vertices, and draw some "extended output range" given the error limits.

```
VertErr=-[lim ehigh [-lim elow(1); lim ehigh(2)] -lim elow [lim ehigh(1); -lim elow(2)]
VertErr = 2x4
  -0.2000 0.1000 0.1000
                         -0.2000
  -0.2500 -0.2500 0.1500
                         0.1500
ImageVerticesU+VertErr(:, 3) ImageVerticesU+VertErr(:, 4)];
keu=convhull(ExtendedImageU(1,:),ExtendedImageU(2,:));
fill(ExtendedImageU(1, keu), ExtendedImageU(2, keu), [1 .4 .5]) %feasible polyhedron + error
fill \, (ImageVerticesU\, (1,k)\,, ImageVerticesU\, (2,k)\,, \,'g') \,\,\, \$ feasible \,\, polyhedron \,\,
fill(ImageVerticesd(1, kd), ImageVerticesd(2, kd), 'c')
fill (VertErr(1,:) *.95+ImageVerticesU(1,2), VertErr(2,:) *.95+ImageVerticesU(2,2), [.75 0.5]
hold off, grid on, axis equal
xlabel("y1"), ylabel("y2")
xline(0, 'r'), yline(0, 'r'),
legend("Extended reachable polyhedron (with error)", "Reachable Output Polyhedron '\psi'",
```



D.2) SVD (ellipse) geometry

SVD/pseudo-inverse solutions are reworking of ordinary least squares... and ordinary least squares have no "constraints" (that would be quadprog). To stay within the underlying assumptions of the methodology, the only thing we may have is "weighted" least squares.

We'll scale things and weight the "residual error" and the "control effort" jointly, as follows.

WorstCaseLim=[0.1 0.15]; %smallest error bound for each variable
E_residual=diag(WorstCaseLim)

So, with scaling $u = E_u \cdot u_{scaled}$, $d = E_d \cdot d_{scaled}$, $\epsilon = E_\epsilon \cdot \epsilon_{scaled}$, where ϵ is the residual output error $\epsilon = G \cdot u_{opt} + Hd \dots$ when, later on, we do know what u_{opt} should be.

The scaled version of the above would be:

$$\epsilon_{scaled} = G_{scaled} u_{opt,scaled} + H_{scaled} d_{scaled}$$

Note that the E_{ε} matrix is an OUTPUT scaling matrix. For "total" disturbance rejection this scaling was not relevant (results would be identical irrespective of the chosen scaling), but this is no longer the case and the scaling is of course important here, to guide the weighted least squares optimization.

Our goal will be achieving $\|\epsilon_{scaled}\|^2 + \|u_{scaled}\|^2 \le 1$, because in that case we can guarantee that both $\|\epsilon_{scaled}\|$ and $\|u_{scaled}\|$ are below 1.

If we denote $\nu = \begin{pmatrix} \epsilon_{scaled} \\ u_{scaled} \end{pmatrix}$, then our goal is achieving $\|\nu\|^2 \le 1$ when $\|d_{scaled}\| \le 1$.

The equations for ν are:

$$\nu = \binom{G_{scaled}}{I_{3\times 3}} u_{scaled} + \binom{H_{scaled}}{0_{3\times 2}} d_{scaled} = T \cdot u_{scaled} + Q \cdot d_{scaled}$$

so the least-squares fit seeking $Tu_{scaled} \approx -Qd_{scaled}$, i.e., minimising $\|\nu\|$, will involve the pseudo-inverse T^{\dagger} of the matrix T multiplying u_{scaled} ,

$$u_{opt,scaled} = -T^{\dagger} \cdot Qd_{scaled}$$

and, as a result, the minimum-norm ν (optimal solution) would be:

$$\nu_{opt} = (-TT^{\dagger}Q + Q)d_{scaled} = (I - TT^{\dagger})Q \cdot d_{scaled}$$

so a sufficient condition for our goal to be feasible is that the maximum singular value (maximum gain) of $(I - TT^{\dagger})Q$ is less than one.

Let's do it:

```
G2esc=inv(E_residual)*Gain*Eu;
H2esc=inv(E_residual)*dcgain(H)*Ed;
T=[G2esc;eye(3)]
```

```
Q=[H2esc; zeros(3,2)]
```

FeedForward2=-pinv(T)*Q %input to FeedForward2 are scaled disturbances, outputs are sca

```
FeedForward2 = 3x2

-0.4806 -0.2259

0.0433 0.0319

0.0002 -0.0898
```

ThingLessThan1=(eye(5)-T*pinv(T))*Q

```
ThingLessThan1 = 5x2
    0.0109    0.0040
    0.0772    0.0523
    -0.4806    -0.2259
    0.0433    0.0319
    0.0002    -0.0898

wcgnu=svd(ThingLessThan1) %Feasible if max gain < 1

wcgnu = 2x1
    0.5431
    0.0828

1/wcgnu(1) %disturbances could be larger by this factor while keeping feasibility

ans = 1.8413
```

NOTE: the extension of these ideas to the frequency domain, even with different frequency-dependent maximum residual error and manipulated variable sizes, gives rise to \mathcal{H}_{∞} control.

*Optional discussion: If we separately analyse error and control action size, we may have a slightly finer picture:

```
wcerr=max( svd(ThingLessThan1(1:2,:)) )
wcerr = 0.0940

wcu=max( svd(ThingLessThan1(3:5,:)) )
wcu = 0.5351

1/wcu %so we have this larger disturbance size margin
ans = 1.8690
```

Indeed, if we could minimise "max (wcerr, wcu)" with a different FeedForward2 matrix, that would be a better solution, closer to the "exact" polyhedron manipulations... but such option is, in principle, out of reach for basic SVD/pseudo-inverse techniques.

In fact, as we want element-by-element less-than-1 results, we could do SVD row by row (which is the same as the Euclidean norm of the row, by the way):

```
for i=1:5
    svd(ThingLessThan1(i,:))
end

ans = 0.0116
ans = 0.0933
ans = 0.5310
ans = 0.0538
```

```
ans = 0.0898
```

This would be the largest margin, in which $u_{1,opt}$ would have size 1 for some disturbance in the unit sphere:

```
1/0.5310
```

ans = 1.8832

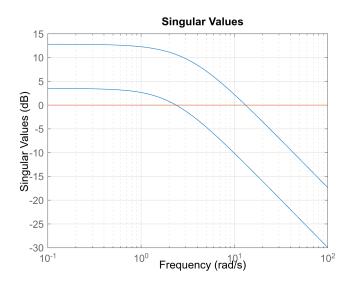
E) Transient analysis (bandwith), setpoint and disturbance

We need the "sigma" singular value plot in frequency, with suitable scalings:

```
Gesc=ss(inv(Ey)*G*Eu); %dynamic system object, not just gain as in earlier sections Hesc=ss(inv(Ey)*H*Ed); %dynamic system object
```

• **Setpoint tracking**, check frequencies above 0dB:

sigma(Gesc,tf(1)), grid on %el eje vert. tiene unidades logarítmicas de "salidas escala



We can track arbitrary setpoints up to 2.4 rad/s bandwith (with the maximum amplitudes implied in the scaling, of course).

Is the manoeuvre at 2.4 rad/s the same as in steady state?

```
Gbw=evalfr(Gesc, 2.374*1j)
```

 $Gbw = 2 \times 3 complex$

```
0.4790 - 0.5685i
                    0.0012 - 0.0058i -0.6890 + 0.4907i
  0.8302 - 0.9855i -0.1005 + 0.2385i
                                        2.5212 - 1.7956i
[Ubw,Sbw,Vbw]=svd(Gbw) %yes, it is... Ubw is close to original U.
Ubw = 2 \times 2 complex
  0.1592 + 0.0000i
                     0.9873 + 0.0000i
  -0.9873 - 0.0002i
                     0.1592 + 0.0000i
Sbw = 2x3
   3.4023
                  0
                            0
             1.0002
        0
                            0
Vbw = 3x3 complex
                    0.6049 + 0.7181i
  -0.2185 - 0.2594i
                                        0.0348 - 0.0477i
                                        0.7896 - 0.6079i
  0.0292 + 0.0695i
                   -0.0148 - 0.0322i
```

0.0204 - 0.0551i

• TOTAL Disturbance rejection, check frequencies below 0dB in:

-0.7637 - 0.5441i -0.2790 - 0.1986i

0.0461

-0.0131

0.0338

-0.0989

```
FF=minreal(-Gesc'*inv(Gesc*Gesc')*Hesc); %pseudoinverse is not made by control systems
12 states removed.

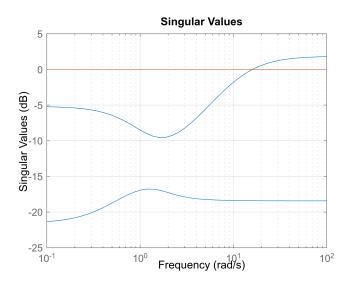
size(FF) %two "d" enter, three MV outputs

State-space model with 3 outputs, 2 inputs, and 8 states.

dcgain(FF)

ans = 3×2
   -0.4930   -0.2343
```

sigma(FF, tf(1)), grid on %vertical axis has logarithmic units of "scaled input".



We have power to cancel the disturbance effect at any frequency below 15 rad/s... in an ideal situation where disturbances were measurable, we had no modelling errors, etc... and we are not limited by measurement noise, delay or whatever: it's an optimistic estimate.

Combined setpoint + disturbances (simultaneously, but norm 1)

If we assume $||r||^2 + ||d||^2 \le 1$, (in scaled units), we can plot the required input amplitude at each frequency, as follows:

```
PinvG=(Gesc'*inv(Gesc*Gesc')); %pseudoinverse is not made by control systems toolbox Preal2=(Gesc'*inv(Gesc*Gesc')*[-Hesc eye(2)]); %pseudoinverse is not made by control system size(Preal2) %two "d" and two "r" enter, three MV outputs
```

State-space model with 3 outputs, 4 inputs, and 20 states.

```
%sigma(Preal2), grid on
sigma(Preal2, tf(1),'-.',FF,PinvG), grid on %vertical axis has logarithmic units of "so
ylim([-30 40]), legend("ref+d","0dB","only d","only r")
```

